

TECHNICAL DATA

# 3A, 30V Synchronus Rectified Step Down Converter

### **General Description**

FTD2786 is a 3A synchronous buck converter with integrated power MOSFETs. The FAC2786 design with a current-mode control scheme, can convert wide input voltage of 4.5V to 30V to the output voltage adjustable from 0.92V to 28V to provide excellent output voltage regulation.

The FAC2786 is equipped with an automatic PFM/PWM mode operation. At light load, the IC operates in the PFM mode to reduce the switching losses. At heavy load, the IC works in PWM mode.

The FAC2786 is also equipped with Power-on-reset, soft- start, and whole protections (over-temperature, and current-limit) into a single package.

This device, available SOP-8E provides a very compact system solution external components and PCB area.

### **Features**

Wide Input Voltage from 4.5V to 30V

 $\overline{a}$ 

- 3A Continuous Output Current
- Adjustable Output Voltage from 0.92V to 28V
- **•** Integrated N-MOSFET
- Fixed 340kHz Switching Frequency
- **•** PFM/PWM mode Operation
- **Stable with Low ESR Capacitors**
- Power-On-Reset Detection
- **•** Programmable Soft-Start
- Over-Temperature Protection
- Over-Voltage Protection
- Current-Limit Protection with Frequency Foldback
- Enable/Shutdown Function
- Lead Free and Green Devices Available(RoHS Compliant)

### **Applications**

- Distributed Power Systems
- Networking Systems
- FPGA, DSP, ASIC Power Supplies
- Green Electronics/ Appliances
- Notebook Computers

### **Pin Configurations**



Figure1 Pin Configuration of FAC2786FE (Top View)



# **Pin Description**



# **Ordering Information**





### **Function Block**



#### **Figure 2 Function Block Diagram of FAC2786**

### **Absolute Maximum Ratings**







# **Recommended Operating Conditions**



### **Electrical Characteristics**

VIN =12V, Vout=3.3V, VEN=3V,TA =+25℃, unless otherwise noted







# **Typical Application Circuit**



\* For cirtical condition, like plug in, the large capacitace and high voltage rating are needed to avoid the high spike voltage.

#### Recommended Feedback Compensation Value





# **Typical Performance Characteristics**

Refer to the "Typical Application Circuit" The test conditions are VIN=12V, Vout=3.3V, L1=10mH, C2=22mF, TA= 25°C unless otherwise specified.



### **Efficiency vs. Output Current**



Soft Start Time vs. SS pin to GND **Capacitance** 







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**Foldback**  $\tilde{v}_{\rm eff}$  $\blacksquare$ ò. MWWW 31  $V_{IR}$  =12V, V<sub>OU</sub> =3.3V, G<sub>OU</sub> =22uF, L=10uH, Ramp up lou- into current limit CH1: VEN, SV/Div, DC CH2:  $V_{\text{L}X}$ , 10V/Div, DC CH3: I., 2A/Div. DC TIME: 50ps/Div

**Current Limit & Frequency** 



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Power Off





**Load Transient** 





CH2: I<sub>OUT</sub>, 2A/Div, DC TIME: 50µs/Div

**Short Circuit** 





### Main Control Loop

The FAC2786 is a constant frequency current mode switching regulator. During normal operation, the internal N-channel power MOSFET is turned on each cycle when the oscillator sets an internal RS latch and would be turned off when an internal current comparator (ICMP) resets the latch. The peak inductor current at which ICMP resets the RS latch is controlled by the voltage on the COMP pin, which is the output of the error amplifier (EAMP). An external resistive divider connected between VOUT and ground allows the EAMP to receive an output feedback voltage VFB at FB pin. When the load current increases, it causes a slight decrease in VFB relative to the 0.92V reference, which in turn causes the COMP volt- age to increase until the average inductor current matches the new load current.

VIN Power-On-Reset (POR) and EN

#### Under-voltage Lockout

The FAC2786 keep monitoring the voltage on VIN pin to prevent wrong logic operations which may occur when VIN voltage is not high enough for the internal control circuitry to operate. The VIN POR has a rising threshold of 4.1V (typical) with 0.5V of hysteresis.

An external under-voltage lockout (UVLO) is sensed at the EN pin. The EN UVLO has a rising threshold of 2.5V with 0.2V of hysteresis. The EN pin should be connected a resistor divider from VIN to EN.

After the VIN and EN voltages exceed their respective voltage thresholds, the IC starts a start-up process and then ramps up the output voltage to the setting of output voltage

### Over-Temperature Protection (OTP)

The over-temperature circuit limits the junction temperature of the FAC2786. When the junction temperature exceeds  $T_J = +160^\circ C$ , a thermal sensor turns off the power MOSFET, allowing the devices to cool. The thermal sensor allows the converter to start a start-up process and regulate

the output voltage again after the junction temperature cools by  $50^{\circ}$  C.

The OTP is designed with a  $50^{\circ}$ C hysteresis to lower the average T<sub>J</sub> during continuous thermal overload conditions, increasing lifetime of the lC.

#### Enable / Shutdown

Driving EN to ground places the FAC2786 in shutdown. When in shutdown, the internal power MOSFET turns off, all internal circuitry shuts down

#### Current-Limit Protection

The FAC2786 monitors the output current, flowing through the N-Channel power MOSFET, and limits the IC from damages during overload, short-circuit and over voltage conditions.

### Frequency Foldback

The foldback frequency is controlled by the FB voltage. When the FB pin voltage is under 0.6V, the frequency of the oscillator will be reduced to 110kHz. This lower frequency allows the inductor current to safely discharge, thereby preventing current runaway. The oscillator's frequency will switch to its designed rate when the feedback voltage on FB rises above the rising frequency foldback threshold (0.6V, typical) again

### Over-Voltage Protection

The over-voltage function monitors the output voltage by FB pin. When the FB voltage increases over 120% of the reference voltage, the over-voltage protection comparator will force the low-side MOSFET gate driver high. This action actively pulls down the output voltage. As soon as the output voltage is within regulation, the OVP comparator is disengaged. The chip will restore its normal operation.



### **Application Information**

### Setting Output Voltage

The regulated output voltage is determined by:

R R

To prevent stray pickup, please locate resistors R1 and R2 close to TD2786.

### Inductor Capacitor Selection

Use small ceramic capacitors for high frequency decoupling and bulk capacitors to supply the surge current needed each time the N-channel power MOSFET (Q1) turns on. Place the small ceramic capacitors physically close to the VIN and between the VIN and GND.

The important parameters for the bulk input capacitor are the voltage rating and the RMS current rating. For reliable operation, select the bulk capacitor with voltage and current ratings above the maximum input voltage and largest RMS current required by the circuit. The capacitor voltage rating should be at least 1.25 times greater than the maximum input voltage and a voltage rating of 1.5 times is a conservative guideline. The RMS current (IRMS) of the bulk input capacitor is calculated as the following equation:

 $I_{RMS} = I_{OUT} \sqrt{D \times (1 - D)}$ 

where D is the duty cycle of the power MOSFET.

For a through hole design, several electrolytic capacitors maybe needed. For surface mount designs, solid tantalum capacitors can be used, but caution must be exercised with regard to the capacitor surge current rating.





### Output Capacitor Selection

An output capacitor is required to filter the output and supply the load transient current. The filtering requirements are the function of the switching frequency and the ripple current (DI). The output ripple is the sum of the voltages, having phase shift, across the ESR and the ideal output capacitor. The peak-to-peak voltage of the ESR is calculated as the following equations:

$$
D = \frac{V_{OUT}}{V_{IN}}
$$

$$
\Delta I = \frac{V_{OUT} \times (1 + D)}{F_{OSC} \times L}
$$

 $V_{ESR} = \Delta I \times ESR$ 

The peak- to-peak voltage of the ideal output capacitor is calculated as the following equations:

$$
\Delta V_{\text{COUT}}\ = \frac{\Delta I}{8\times F_{\text{OSC}}\times C_{\text{OUT}}}
$$

For the applications using bulk capacitors, the VCOUT is much smaller than the VESR and can be ignored. Therefore the AC peak-to-peak output voltage ( $\Delta V_{\text{OUT}}$ ) is shown below:

 $\Delta V_{\text{OUT}} = \Delta I \times ESR$ 

For the applications using bulk capacitors, the VESR is much smaller than the  $\Delta$  Vcout and can be ignored Therefore, the AC peak-to-peak output voltage( $\Delta$  Vout) is to  $\Delta$  Vcout



### Output Capacitor Selection

The load transient requirements are the function of the slew rate (di/dt) and the magnitude of the transient load current. These requirements are generally met with a mix of capacitors and careful layout. High frequency capacitors initially supply the transient and slow the current load rate seen by the bulk capacitors. The bulk filter capacitor values are generally determined by the ESR and voltage rating requirements rather than actual capacitance requirements.

High frequency decoupling capacitors should be placed as close to the power pins of the load as physically possible. Be careful not to add inductance in the circuit board wiring that could cancel the usefulness of these low inductance components. An aluminum electrolytic capacitor's ESR value is related to the case size with lower ESR available in larger case sizes. However, the Equivalent Series Inductance (ESL) of these capacitors increases with case size and can reduce the usefulness of the ca- pacitor to high slew-rate transient loading.

**Table1 Capacitor Selection Guide** 



#### Inductor Value Calculation

The operating frequency and inductor selection are interrelated in that higher operating frequencies permit the use of a smaller inductor for the same amount of inductor ripple current. However, this is at the expense of efficiency due to an increase in MOSFET gate charge losses. The equation shows that the inductance value has a direct effect on ripple current.

Accepting larger values of ripple current allows the use of low inductances, but results in higher output voltage ripple and greater core losses. A reasonable starting point for setting ripple current is  $\Delta$ I $\leq$ 0.4 x Iout(max). Please be noticed that the maximum ripple current occurs at the maximum input voltage. The minimum inductance of the inuctor is calculated by using the following equation:

$$
\frac{V_{\text{OUT}} \times (V_{\text{IN}} - V_{\text{OUT}})}{340000 \times L \times V_{\text{IN}}} \le 1.2
$$

$$
L \ge \frac{V_{\text{OUT}} \times (V_{\text{IN}} - V_{\text{OUT}})}{408000 \times V_{\text{IN}}}
$$

Where  $V_{IN} = V_{IN(MAX)}$ 

Table2 Inductor Selection Guide





# **Package Information**

**SOP-8E Package Outline Dimensions** 







